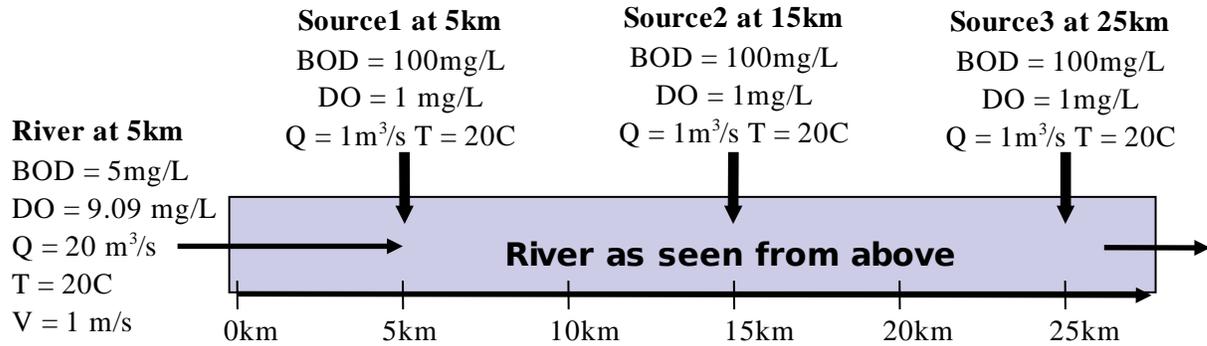


PROBLEM 1 (20 pts):



There are a great many BOD sources that affect the water quality of surface waters near urban areas. In this problem, three urban runoff sources enter a river through CSOs during a rainfall event, as illustrated above.

(a) Give the general assumptions associated with applying the Streeter-Phelps model here:

1. Are concentrations steady? *Yes*
2. Are concentrations uniform? *No (as we go downstream, BOD jumps where there are sources and decreases over stretches where there are no sources)*
3. Other assumptions? *First-order decay for BOD and first-order aeration with uniform rate constants; constant water temperature, salinity, and velocity; no other inflows/outflows, or reactions of BOD or DO*

(b) Sketch qualitatively river BOD and DO as functions of x between 0km and 25km. Do not calculate anything, but do label the curves so it is clear which is for BOD and which is for DO. BOD decreases exponentially between sources and jumps at the source locations. DO does not show such jumps; only its downward slope become steeper. DO tends to decrease when VOD is high (more deoxygenation) and increase when DO is low (more reoxygenation).

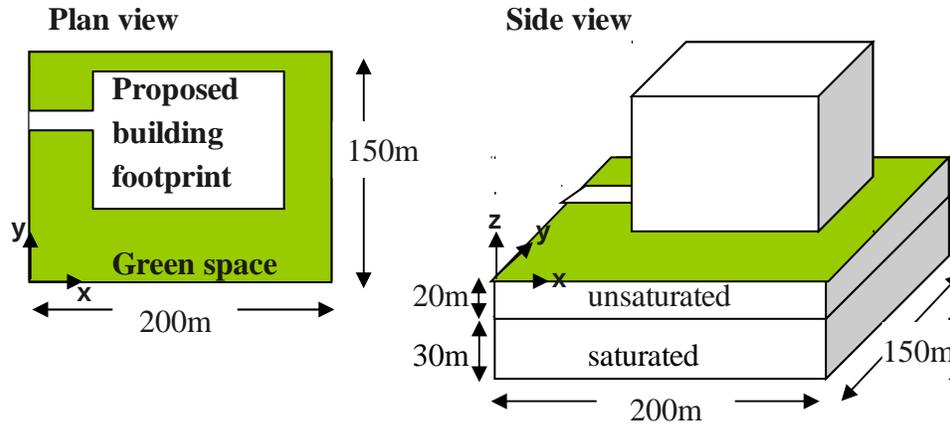
(c) Determine the concentration of BOD and DO at 10km if $k_d(20C) = 0.2 \text{ d}^{-1}$, $k_r(20C) = 0.8 \text{ d}^{-1}$. The transit time from the initial condition at $x = 5\text{km}$ is $t = \Delta x/v = 5000 \text{ s}$. The initial condition (mixing of inflow and Source 1) has $Q = 21 \text{ m}^3/\text{s}$, $L = 9.5 \text{ mg/L}$, $DO = 8.70 \text{ mg/L}$ ($D = 0.39 \text{ mg/L}$), $T = 20C$.

Because there is no source of BOD between 5 and 10 km, the BOD concentration is given by exponential decay: $L(t) = L_0 e^{-k_d t} = 9.4 \text{ mg/L}$.

The DO concentration is given by

$$DO(t) = DO_{\text{sat}}(T) - \frac{k_d L_0}{k_r - k_d} [e^{-k_d t} - e^{-k_r t}] - D_0 e^{-k_r t} = 8.62 \text{ mg/L}.$$

PROBLEM 2 (20 pts):



Engineers are estimating the area of green space needed for a new housing development to meet NYC's policy to increase infiltration and reduce runoff.

Borings reveal that both the unsaturated and saturated zone soils are made up of Carnegie sandy loam, with $f_c = 4.50$ cm/h, $f_o = 35.52$ cm/h, $k = 19.64$ /h, $K = 0.4$ m/day, $\eta = 0.3$, $\rho = 1400$ kg/m³, $f_{oc} = 0.005$.

Determine the amount of exposed soil (green space), as an area and as a percentage of the lot area, needed to infiltrate 750 m³ water over the first 30 minutes of a rainstorm.

Infiltration expression over the rainstorm: $f(t) = f_c + (f_o - f_c)e^{-kt}$

Integrated amount from time 0 to T:

$$\int_0^T (f_c + (f_o - f_c)e^{-kt}) dt = \left[f_c t - \frac{f_o - f_c}{k} e^{-kt} \right]_0^T = f_c T + \frac{f_o - f_c}{k} (1 - e^{-kT}).$$

With the given parameter values, this works out to 3.83 cm infiltration over the first 0.5 h. With this infiltration rate, we would need $750 \text{ m}^3 / 0.0383 \text{ m} = 1.96 \times 10^4 \text{ m}^2$ soil surface area to infiltrate the required amount of water. This corresponds to 65% of the lot area, which is $3 \times 10^4 \text{ m}^2$.

PROBLEM 3 (20 pts):

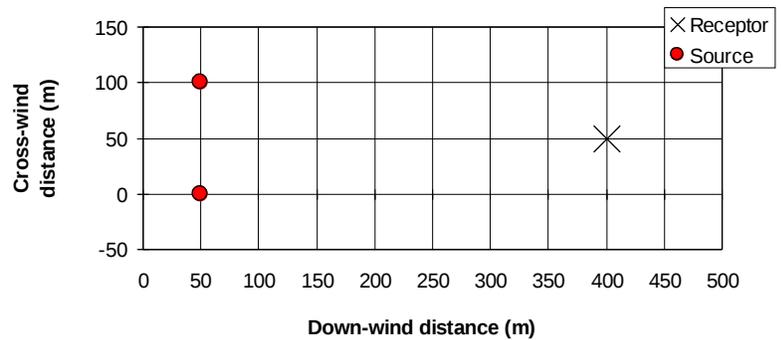
Silica fume is often mixed into concrete for strength. It is a fine powder and can easily become suspended in the air during mixing as PM_{2.5}.

Wind speed at 10m is 5 m/s.

Upwind PM_{2.5} concentration is 10 µg/m³.

The atmospheric stability class is B between 0 and 300m above ground, and F above 300m.

The two emission sources are identical, each with emission rate of 0.5 g/s and an effective height (h+Δh) of 10m.



Use the Gaussian Plume model to estimate the PM_{2.5} concentration at the receptor (in g/m³). Be sure to determine which form of the Gaussian Plume model to use first. Specify any assumptions you are making in applying the GPM.

Plume parameters from table (x < 1 km): a = 156, c = 106.6, d = 1.149, f = 3.3

Plume dimensions (for each source, x = 0.35 km): $\sigma_y = a x^{0.894} = 61 \text{ m}$, $\sigma_z = c x^d + f = 35 \text{ m}$.

Check for effect of the inversion starting at L = 300 m: $x_L = \left(\frac{0.47(L-H)-f}{c} \right)^{1/d} = 1.21 \text{ km}$ (1.22

km if we redo with the x > 1 km plume parameter values), so plumes are not affected at receptor.

Because the 2 sources are effectively the same distance and direction from the receptor (x = 0.35 km, |y| = 50 m), the concentration due to each one will be the same. This is (assuming that all of the emitted silica fume is PM_{2.5})

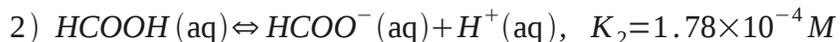
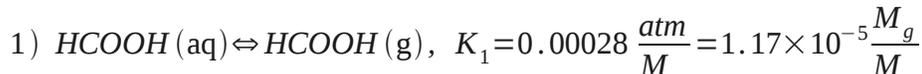
$$C(x,y,0) = \frac{E}{\pi u_H \sigma_y \sigma_z} \exp\left[-\frac{1}{2}\left(\frac{y}{\sigma_y}\right)^2\right] \exp\left[-\frac{1}{2}\left(\frac{H}{\sigma_z}\right)^2\right] = 1.02 \times 10^{-5} \text{ g m}^{-3}.$$

Doubling this and adding the background concentration, and assuming that the PM_{2.5} concentration doesn't change due to reaction, we get $C_{x,y,0}^{\text{total}} = C_u + 2C_{x,y,0}^{\text{plume}} = 3.03 \times 10^{-5} \text{ g m}^{-3}$.

PROBLEM 4 (20 pts):

When traffic gets rerouted around a project site, some communities can experience more traffic than usual. In this problem, you will estimate the impact of formic acid, $\text{HCOOH}(\text{g})$, emissions from rerouted vehicles on water quality at a nearby lake.

The ONLY two relevant reactions are:



- a) Write the equilibrium rate expression for the two reactions that are given above, using “*” to show concentrations at equilibrium.

Products over reactants:

$$\frac{[\text{HCOOH}(\text{g})]^*}{[\text{HCOOH}(\text{aq})]^*} = K_1 = 0.00028 \frac{\text{atm}}{\text{M}} = 1.17 \times 10^{-5} \frac{\text{M}_g}{\text{M}}$$

$$\frac{[\text{HCOO}^-(\text{aq})]^* [\text{H}^+(\text{aq})]^*}{[\text{HCOOH}(\text{aq})]^*} = K_2 = 1.78 \times 10^{-4} \text{M}$$

- b) If the equilibrium pH is 5 and the equilibrium concentration of HCOOH_g in the air is $4.16 \times 10^{-11} \text{M}_g = 10^{-9} \text{atm}$, determine the equilibrium concentrations of HCOOH_{aq} and $\text{HCOO}^-_{\text{aq}}$ in the lake in M. Assume that the air CV is $85,000,000 \text{m}^3$ and the water CV is $125,000 \text{m}^3$.

$$[\text{HCOOH}(\text{aq})]^* = \frac{[\text{HCOOH}(\text{g})]^*}{K_1} = 3.56 \times 10^{-6} \text{M}$$

$$[\text{HCOO}^-(\text{aq})]^* = \frac{[\text{HCOOH}(\text{aq})]^* K_2}{[\text{H}^+(\text{aq})]^*} = 6.33 \times 10^{-5} \text{M}$$

PROBLEM 5 (20 pts):

Below are extracts from the EIS for the Cape Wind offshore wind energy project, completed by the US Department of the Interior in 2009. Based on the information given as well as on what you learned in class and in your group project,

(a) Concisely describe the project alternatives that were analyzed, and explain how these relate to EQR requirements.

Alternatives included the proposed project; No-Action (as required); changing the wind farm location (partly suggested by public and agency comments); and reducing the size of the project, doing it in two phases, or concentrating the turbines over a smaller area.

(b) Concisely describe the main potential impacts of the project (which may be negative and/or positive) on the attributes of (1) Natural Resources, (2) Transportation, (3) Air Quality, (4) Greenhouse Gas Emissions.

Natural resources: disturbance of aquatic life, particularly organisms living on the seabed, by laying down the turbine foundations and power lines

Transportation: Possible traffic delays in the construction phase from bringing heavy equipment and components to the project port; commutes of the construction and maintenance crews may bring more traffic to small towns.

Air quality: Emission-free power source that would eliminate pollution associated with displaced fossil fuel electricity generation, but some emissions from diesel engines for construction and maintenance equipment and barges.

GHG emissions: Similar to air quality: eliminate pollution associated with displaced fossil fuel electricity generation, but some (probably much lesser) emissions from diesel engines for construction and maintenance equipment and barges.